

Resistor Programmable Universal Active Filter

Data Sheet

MSU1F1/4, MSU2F1

Description

The resistor programmable universal active filter is a CMOS chip that can be configured for Lowpass, Bandpass, Highpass, Elliptic, Notch or Allpass filters using external resistors. The filters come in one (8 pin) or two (16 pin) section versions. The device is a switched-capacitor filter using a topology that requires fewer pins and less power consumption than other switched-capacitor universal active filters. The clock to corner ratio as well as the Q are set by external resistors.

Depending on the filter type and response, from zero to nine external resistors are needed for each section. The sections may be cascaded to realize higher order filters.

The devices have a selectable nominal sample to corner ratio of either 50 to 1 or 100 to 1 and come in either a low power version ($f_o < 3$ kHz) or a higher power version ($f_o < 20$ kHz). With device current as low as 50 μ A per section, the chip is ideal for low power and portable application. The devices are double sampled to reduce the clock frequency by a factor of two.

Features

Low Power Consumption
 Low Voltage Operation 3.0V to 5.5V
 Low Cost
 Small Package Size 8 or 16 pin DIP or SOIC
 Wide Q Range 0.5 to over 200
 Wide Clock to Center/Corner Frequency Range 25:1 to over 200:1
 Accurate Switched-Capacitor Technology

Applications

General Purpose Filtering
 Portable Equipment
 Instrumentation

Absolute Maximum Ratings

Power Supply Voltage +6V
 Storage Temperature -60 to +150°C
 Operating Temperature 0 to 70°C

Ordering Information

Part Number	Package	Operating Temperature
MSU1F1P	8 Pin DIP	0 - 70°C
MSU1F1S	8 Pin SOIC	0 - 70°C
MSU1F2P	8 Pin DIP	0 - 70°C
MSU1F2S	8 Pin SOIC	0 - 70°C
MSU1F3P	8 Pin DIP	0 - 70°C
MSU1F3S	8 Pin SOIC	0 - 70°C
MSU1F4P	8 Pin DIP	0 - 70°C
MSU1F4S	8 Pin SOIC	0 - 70°C
MSU2F1P	16 Pin DIP	0 - 70°C
MSU2F1S	16 Pin SOIC	0 - 70°C

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Electrical Characteristics

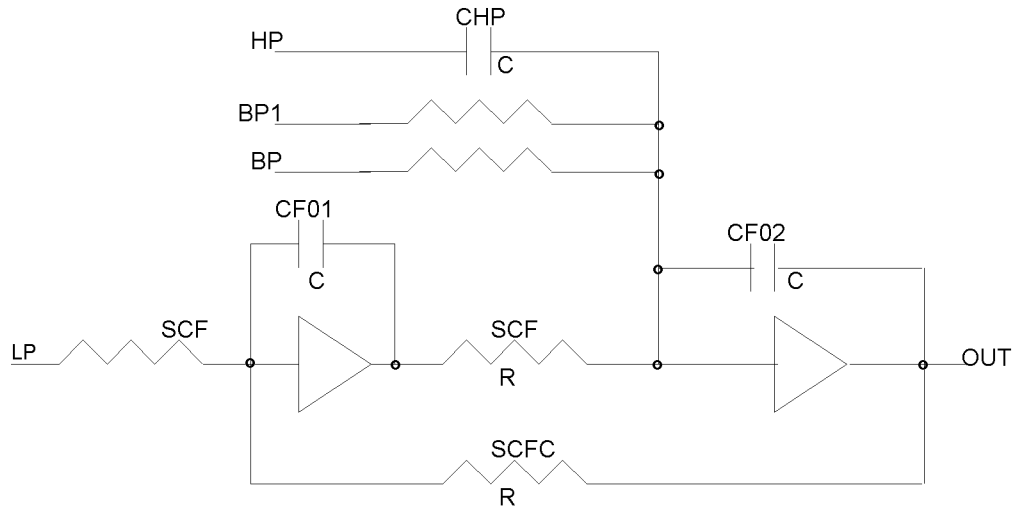
(VDD = +5V, T + 25 °C)

PARAMETER	SYMBOL	CONDITONS	MIN	TYP	MAX	UNITS
DC Specifications						
Operating Voltage	VDD		3.0	5.0	5.5	V
Supply Current	IDD	MSU2F1 PWR=1	100	200	300	μ A
		MSU2F1 PWR=0	500	1000	2000	μ A
		MSU1F1/3	50	100	200	μ A
		MSU1F2/4	250	500	1000	μ A
Output Impedance			700			Ω
Output Offset				20		mV
AC Specifications						
Output Swing			4.0	4.5		Vp-p
Input Impedance	Zin			1		M Ω
Nominal Clock to corner	Fo	MSU2F1 FO=1		25		
		FO=0		50		
		MSU1F1/2		25		
		MSU1F3/4		50		
Center/Corner Range note (1)		MSU2F1 PWR=1	3	6		kHz
		PWR=0	20	40		kHz
		MSU1F1/3	3	6		kHz
		MSU1F2/4	20	40		kHz
Clock Input Voltage	Ckin		0.1	note(2)	5	Vp-p

note(1): the sample to corner ratio is twice the clock to corner ratio

note(2): 100mV sine wave clock requires capacitive coupling, and $f_c < 100$ kHz.

Block Diagram



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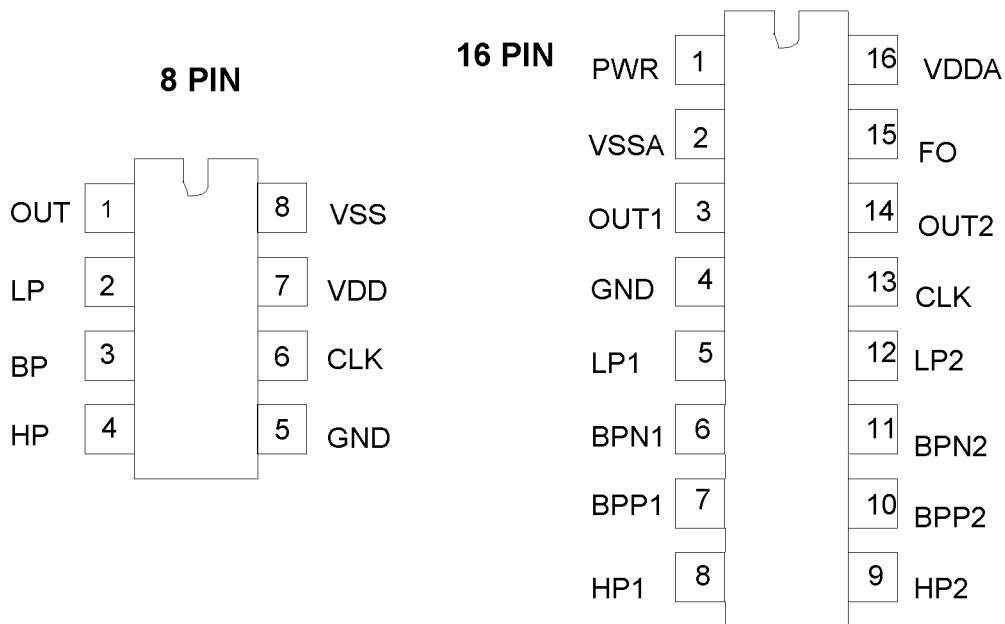
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Pin Description

16 Pin	8 Pin	Pin	Description
1		PWR	Power Select Pin 0 = High 1 = Low
2	8	VSS	Negative Supply, Typically 0V for Single Supply, - 2.5 V for dual supply
3	1	OUT1	Section One Output
4	5	GND	Ground Reference, Typically 2.5V for Single Supply, 0V for dual supply
5	2	LP1	Section One Lowpass Input
6	3	BPN1	Section One Negative Bandpass Input
7		BPP1	Section One Positive Bandpass Input
8	4	HP1	Section One High Pass Input
9		HP2	Section Two High Pass Input
10		BPP2	Section Two Positive Bandpass Input
11		BPN2	Section Two Negative Bandpass Input
12		LP2	Section Two Lowpass Input
13	6	CLK	Input Clock, CMOS Level, Typically 0 - 5V for single, supply 0 - 2.5V for dual supply
14		OUT2	Section Two Output
15		F0 note 1	Clock to Center/Corner, Select Pin, Low = 50 to 1 High = 25 to 1
16	7	VDD	Positive Supply, Typically 5V for single supply, 2.5V for dual supply

Pin Configuration



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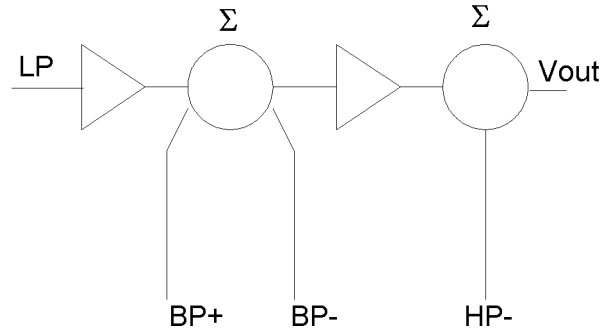
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Filter Types Available

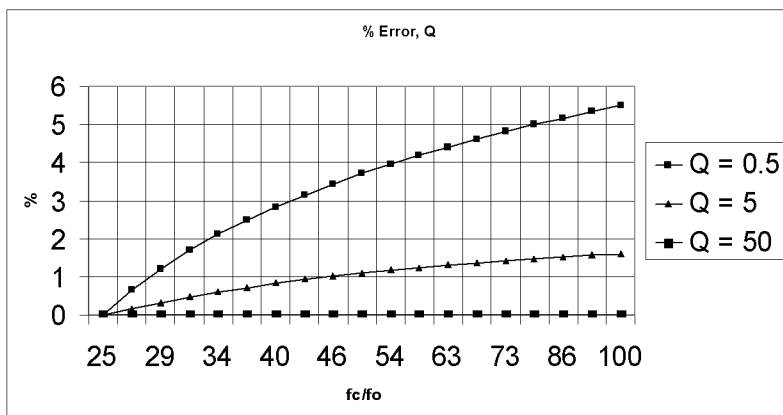
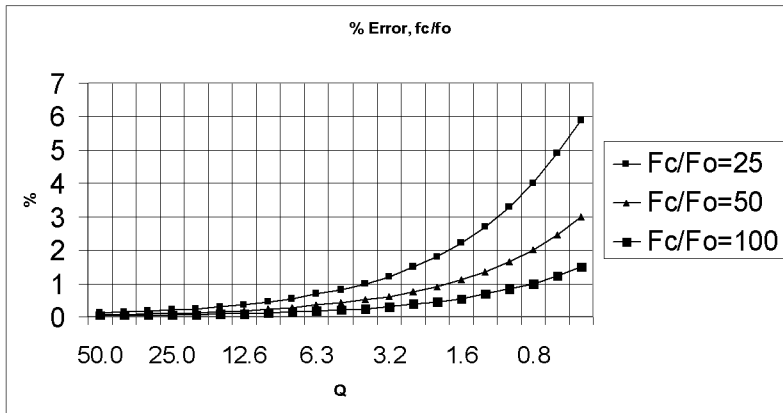
MSU2F1 MSU1F2

Lowpass	yes	yes
Bandpass	yes	yes
Highpass	yes	yes
Lowpass elliptical	yes	yes
Highpass elliptical	yes	yes
Notch	yes	yes
Oscillator	yes	no
Allpass	yes	no
Biquad	yes	no

Block Diagram



Programming Non-Linearities



Transfer Functions

Lowpass

$$H(s) = \frac{\omega_0^2}{s^2 + (\omega_0/Q)s + \omega_0^2}$$

Bandpass

$$H(s) = \frac{-(\omega_0/Q)s}{s^2 + (\omega_0/Q)s + \omega_0^2}$$

Highpass

$$H(s) = \frac{s^2}{s^2 + (\omega_0/Q)s + \omega_0^2}$$

Lowpass Elliptic

$$H(s) = \frac{(\omega_0/\omega_z)^2 s^2 + \omega_0^2}{s^2 + (\omega_0/Q)s + \omega_0^2}$$

Highpass Elliptic

$$H(s) = \frac{s^2 + (\omega_z/\omega_0)^2 \omega_0^2}{s^2 + (\omega_0/Q)s + \omega_0^2}$$

Notch

$$H(s) = \frac{s^2 + \omega_0^2}{s^2 + (\omega_0/Q)s + \omega_0^2}$$

Allpass

$$H(s) = \frac{s^2 - (\omega_0/Q)s + \omega_0^2}{s^2 + (\omega_0/Q)s + \omega_0^2}$$

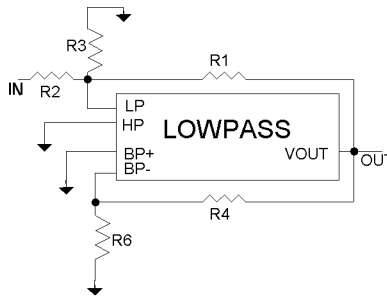
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NOTE: $f_c > 36 \frac{f_o}{\alpha}$

For lowpass, lowpass elliptical, highpass elliptical, allpass and notch filters. This limitation due to the particular ratio of R_1 and R_2 and allows realizable values of R_3 . Other minimum values of f_c/f_o can be obtained by using other values of R_1 and R_2 in the basic biquad equations.

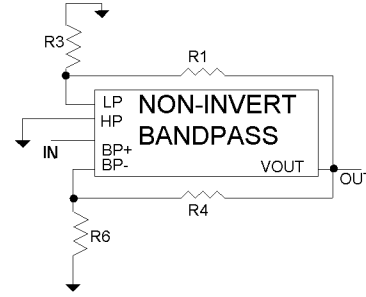


Assumption (1) $R_1 = R_2$; DC Gain = Unity

$$f_0 = \sqrt{K_1''} \frac{f_c}{\alpha} \quad K_1'' = \frac{R_3}{R_1 + R_3}$$

$$Q = \frac{\sqrt{K_1''}}{K_2''} \quad K_2'' = \frac{R_6}{R_4 + R_6}$$

(1) If a gain other than unity is desired then gain = $\frac{R_1}{R_2}$ and K_1'' from the biquad equations should be substituted for K_1''



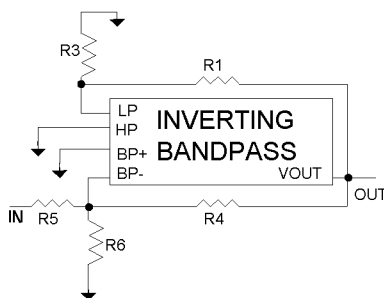
$$\text{Gain}^{(1)} = \frac{1}{K_2'}$$

$$f_0 = \sqrt{K_1''} \cdot \frac{f_c}{\alpha} \quad K_1'' = \frac{R_3}{R_1 + R_3}$$

$$Q = \frac{\sqrt{K_1''}}{K_2'} \quad K_2' = \frac{R_6}{R_4 + R_6}$$

(1) Gain may be adjusted independent of G using the resistor divider described by K_5 from the biquad equations. Use the K_5 equation in place of K_2 for the gain equation only.

where $\alpha = 25:1$ or $50:1$ depending upon the setting of f_o .

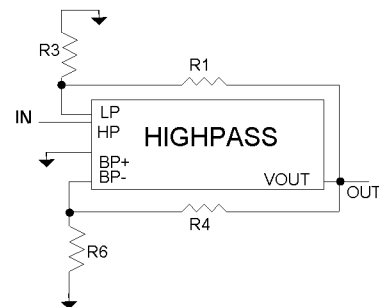


Assumption (1) $R_4 = R_5$; Gain = Unity

$$f_0 = \sqrt{K_1''} \frac{f_c}{\alpha} \quad K_1'' = \frac{R_3}{R_1 + R_3}$$

$$Q = \frac{\sqrt{K_1''}}{K_2''} \quad K_2'' = \frac{R_6}{R_4 + 2R_6}$$

(1) For gains not equal to unity, gain = R_4/R_5 and K_2'' should be replaced with K_2 from the biquad equations.



Gain = Unity

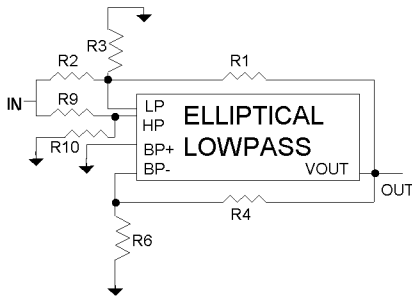
$$f_0 = \sqrt{K_1''} \frac{f_c}{\alpha} \quad K_1'' = \frac{R_3}{R_1 + R_3}$$

$$Q = \frac{\sqrt{K_1''}}{K_2'} \quad K_2' = \frac{R_6}{R_4 + R_6}$$

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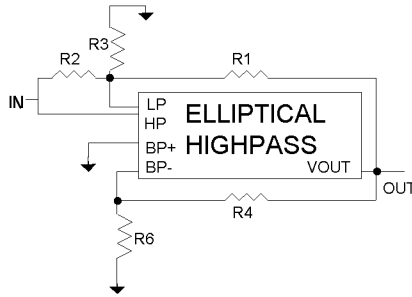
DC Gain (1) = Unity; $R_1 = R_2$

$$f_0 = \sqrt{K_1} \cdot \frac{fc}{\alpha} \quad K_1 = \frac{R_3}{R_1 + R_3}$$

$$Q = \frac{\sqrt{K_1}}{K_2} \quad K_2 = \frac{R_6}{R_4 + R_6}$$

$$f_z = \sqrt{\frac{1}{K_3}} \cdot f_0 \quad K_3 = \frac{R_{10}}{R_9 + R_{10}}$$

- (1) For gain other than unity, gain = R_1/R_2 and K_1 should be substituted for K_1 . The $\sqrt{1/K_3}$ term should also be multiplied by the gain.
- (2) where α is 25 or 50 depending upon the setting of f_0



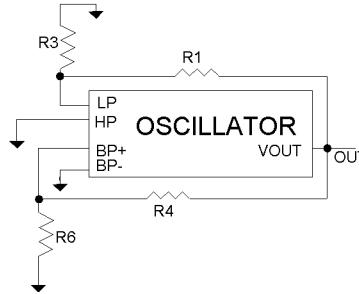
Gain = Unity

$$(1) f_0 = \sqrt{K_1} \cdot \frac{fc}{\alpha}$$

$$Q = \frac{\sqrt{K_1}}{K_2} \quad K_1 = \frac{R_2 R_3}{R_1 R_2 + R_1 R_3 + R_2 R_3}$$

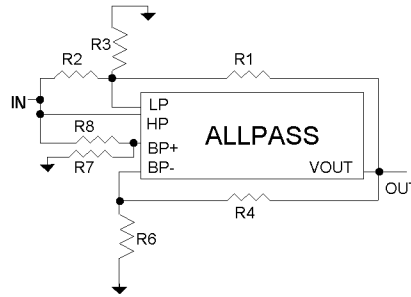
$$f_z = \sqrt{\frac{R_1}{R_2}} \cdot f_0 \quad K_2 = \frac{R_6}{R_4 + R_6}$$

- (1) For this case only, the resistor values R_1 and R_2 should be determined for f_z before the resistor values for f_0 (R_3) are calculated
- (2) where α is 25 or 50 depending upon the setting of f_0



$$(1) f_0 = \frac{\sqrt{R_3}}{\sqrt{R_1 + R_3}} \cdot \frac{fc}{\alpha} \quad (2) \frac{R_4}{R_6} = 20$$

- (1) f_0 is also a function of the feedback coefficient defined by R_4 and R_6 and can vary considerably from the calculated value. For a fixed feedback coefficient, f_0 will not vary by more than plus or minus 1%.
- (2) The distortion of the sine wave can be adjusted by varying this ratio.
- (3) where α is 25 or 50 depending upon the setting of f_0 .



Gain = Unity; $R_1 = R_2$; $R_7 = R_4$; $R_8 = R_6$

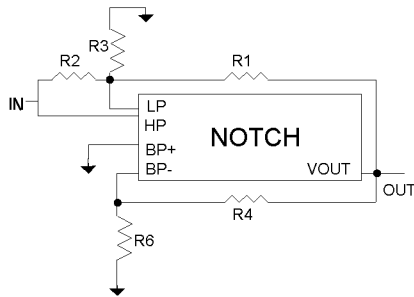
$$f_0 = \sqrt{K_1} \cdot \frac{fc}{\alpha} \quad K_1 = \frac{R_3}{R_1 + 2R_3}$$

$$Q = \frac{\sqrt{K_1}}{K_2} \quad K_2 = \frac{R_6}{R_4 + R_6}$$

- (1) where α is 25 or 50 depending upon the setting of f_0 .

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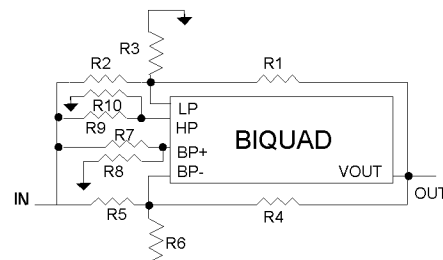
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Gain = Unity, $R_1 = R_2$

$$f_0 = \frac{\sqrt{K_1}}{\alpha} \cdot f_c \quad K_1 = \frac{R_3}{R_1 + 2R_3}$$

$$Q = \frac{\sqrt{K_1}}{K_2} \quad K_2 = \frac{R_6}{R_4 + R_6}$$

where $\alpha = 25:1$ or $50:1$ depending upon the setting of f_0 .



The biquad is the most general purpose filter type. By adjusting the values of K_1 through K_6 , virtually any second order transfer function can be achieved. In some cases, it may be necessary to use an inverting op amp to achieve the correct polarity on these constants.

$$V_{OUT} = V_{IN} \left[-K_3 S^2 - \frac{K_4 S}{4} f_c + \frac{K_5 S}{4} f_c - \frac{K_6}{16} f_c^2 \right]$$

$$K_1 = \frac{R_2 R_3}{R_1 R_2 + R_1 R_3 + R_2 R_3} \quad K_4 = \frac{R_4 R_6}{R_4 R_5 + R_4 R_6 + R_5 R_6}$$

$$K_2 = \frac{R_5 R_6}{R_4 R_5 + R_4 R_6 + R_5 R_6} \quad K_5 = \frac{R_8}{R_7 + R_8}$$

$$K_3 = \frac{R_{10}}{R_9 + R_{10}} \quad K_6 = \frac{R_1 R_3}{R_1 R_2 + R_1 R_3 + R_2 R_3}$$

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STANDARD PRODUCTS

MSGEQ5A	Five Band Graphic Equalizer
MSGEQ7	Seven Band Graphic Equalizer
MSHFS1-6	Selectable High Frequency LP/BP Filter
MSFS1-6	Selectable Lowpass/Bandpass Filter
MSCAHF	Selectable High Frequency Active Lowpass/Bandpass Filter
MSU1F1-4, MSU2F1	Resistor Programmable Universal Active Filter
MSU1HF1-4, MSU2HF1	High Frequency Resistor Programmable Universal Active Filter
MSELP	Switched Capacitor Elliptic Lowpass Filter with Op Amps
MSNBLP	Switched Capacitor Butterworth Lowpass Filter
MSLE/B/C5L/M	Switched Capacitor General Purpose Lowpass Filter
MS2LFS	Dual Selectable Low Voltage Lowpass/Bandpass Filter
MSHN1-6	Selectable High Pass/Notch Filter
MSRAAF	Resistor Programmable Active Audio Filter
MSRAHF	Resistor Programmable Active High Frequency Filter
MS2CAP	Two Channel Audio Processor
MS6CAP	Six Channel Audio Processor

